

Lesson 37: Final Exam Review

Example Problem 1

Calculate the node voltages in the circuit below.

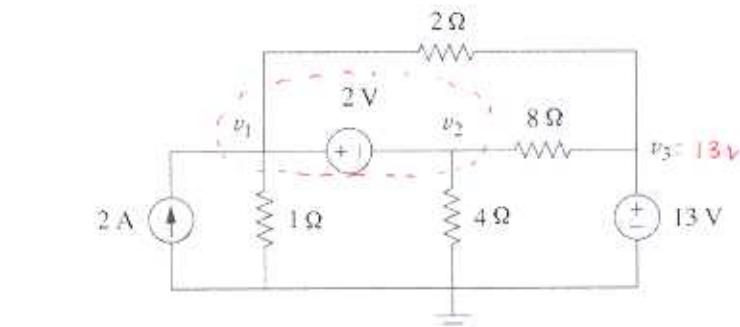
$$KVL \quad v_1 = v_2 + 2$$

$$\frac{v_1 - 3}{2} + \frac{v_2 - 13}{8} + \frac{v_2}{4} + v_1 - 2 = 0$$

$$12v_1 + 3v_2 = 81$$

$$v_1 - v_2 = 2$$

$$\begin{bmatrix} 12 & 3 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} 81 \\ 2 \end{bmatrix} \Rightarrow$$



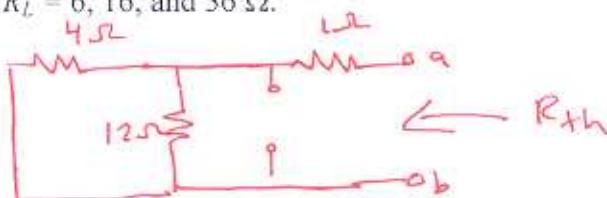
$$v_1 = 5.8V$$

$$v_2 = 3.8V$$

$$v_3 = 13V$$

Example Problem 2

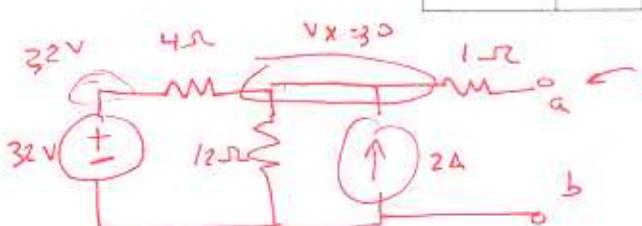
Find the Thévenin equivalent circuit to the left of terminals $a-b$. Then find the current through $R_L = 6, 16$, and 36Ω .



$$R_{th} = 4 \parallel 12 + 1$$

$$= 3 + 1$$

$$R_{th} = 4\Omega$$



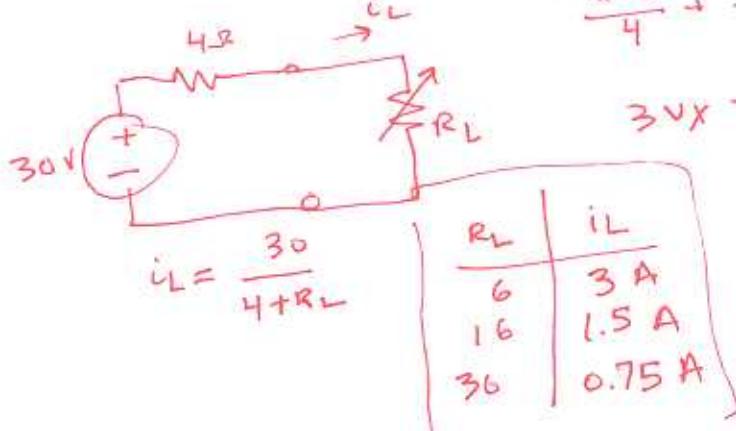
$$\frac{Vx - 32}{4} + \frac{Vx}{12} - 2 = 0$$

$$3Vx - 96 + Vx - 24 = 0$$

$$4Vx = 120$$

$$Vx = 30V$$

$$V_{th} = 30V$$



Example Problem 3

Determine i_x and i_y below.

$$\textcircled{1} \text{ Label output voltage } V_{\text{out}}$$

$$\textcircled{2} \quad V_x = \frac{8k}{8k+2k} \cdot V_{\text{out}} = 0.8 V_{\text{out}}$$

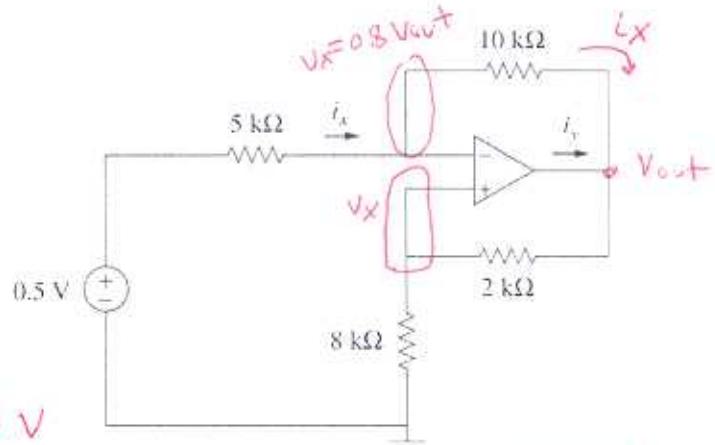
$$\textcircled{3} \text{ KCL at inverting input}$$

$$\frac{0.8 V_{\text{out}} - 0.5}{5k} + \frac{0.8 V_{\text{out}} - V_{\text{out}}}{10k} = 0 \\ \Rightarrow V_{\text{out}} = \frac{5}{7} V = 0.714 V$$

$$\textcircled{4} \quad i_x = \frac{0.5 - 0.8 V_{\text{out}}}{5k} = \frac{0.5 - 0.8(5/7)}{5k} = -0.0143 \text{ mA} = \boxed{-14.3 \mu\text{A}}$$

$$\textcircled{5} \text{ KCL at } V_{\text{out}} \text{ to find } i_y$$

$$i_x + i_y = \frac{V_{\text{out}}}{2k + 8k} \Rightarrow i_y = \frac{0.714 V}{10k} + 0.0143 = \boxed{85.7 \mu\text{A}}$$



Example Problem 4

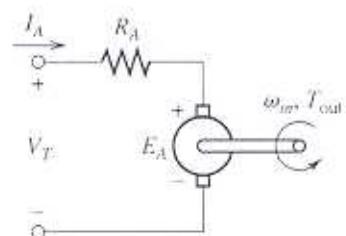
A 120-V permanent magnet DC motor tested under two conditions: loaded and unloaded.

Without a load the speed of the motor ω_m is 160 rad/s and I_A is 1 A. With a load, the speed of the motor ω_m is 148.6 rad/s and I_A is 2 A. Solve for R_A , K_V and T_{loss} .

$$V_T = I_A R_A + K_V \omega$$

$$\text{case 1: } 120 = (1) R_A + K_V \cdot 160$$

$$\text{case 2: } 120 = 2 R_A + K_V \cdot 148.6$$



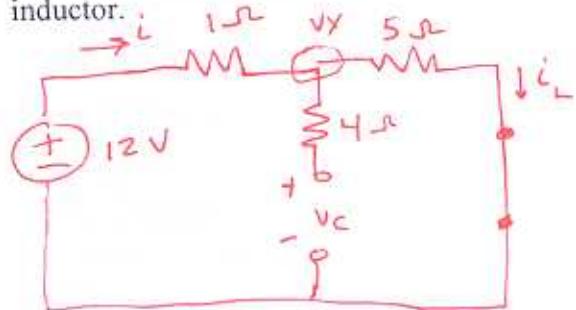
$$\begin{bmatrix} 1 & 160 \\ 2 & 148.6 \end{bmatrix} \begin{bmatrix} R_A \\ K_V \end{bmatrix} = \begin{bmatrix} 120 \\ 120 \end{bmatrix} \Rightarrow \begin{cases} R_A = 7.98 \Omega \\ K_V = 0.7 \text{ V·s} \end{cases}$$

$$\text{Find } T_{\text{loss}} \quad T_{\text{out}}^{\circ} = T_{\text{dev}} - T_{\text{loss}} \quad (\text{case 1: } T_{\text{out}} = 0, \text{ unloaded})$$

$$\Rightarrow T_{\text{dev}} = T_{\text{loss}} = K_V I_A \\ = (0.7)(1 \text{ A}) \\ = \boxed{0.7 \text{ N·m}}$$

Example Problem 5

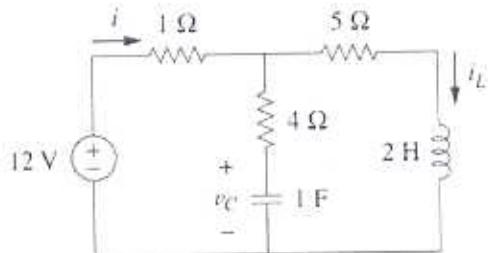
Under dc conditions find i , v_C , and i_L . Also, determine the energy stored in the capacitor and inductor.



$$i = \frac{12V}{1+5} = \frac{12}{6} = 2A$$

$$i_L = 2A$$

$$v_C = v_x = 12 \cdot \frac{5}{5+1} = 10V$$

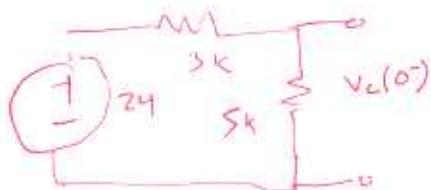


$$w_C = \frac{1}{2} C V^2 \\ = \frac{1}{2} (1F) (10)^2 \\ = 50J$$

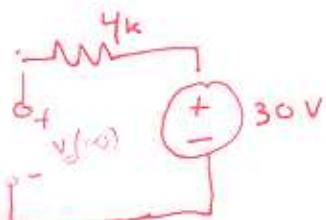
$$w_L = \frac{1}{2} L i^2 \\ = \frac{1}{2} \cdot 2 \cdot 2^2 \\ = 4J$$

Example Problem 6

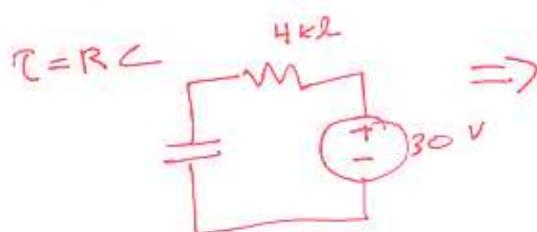
The switch in the circuit below has been in position A for a long time. At $t = 0$, the switch moves to B. Determine $v(t)$ for $t \geq 0$ and calculate its value at $t = 2$ and 4 sec.



$$v_C(0-) = 24 \cdot \frac{5}{5+8} = 15V$$

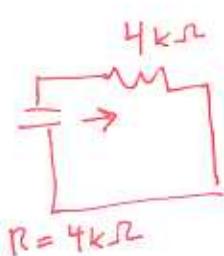


$$v_C(\infty) = 30V$$



$$\tau = R C \\ = (4000)(0.0005 F) \\ = 2sec$$

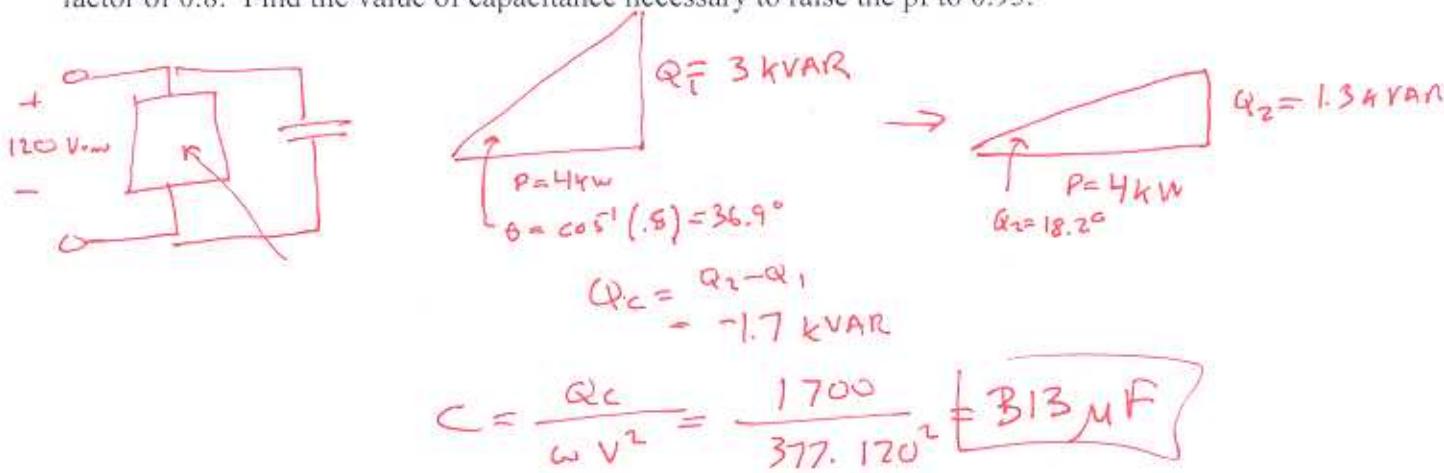
$$v_C(t) = v(\infty) + [v(0) - v(\infty)] e^{-t/\tau} \\ = 30 + [15 - 30] e^{-t/2} \\ = 30 - 15e^{-t/2}$$



$$v_C(2) = 24.48V \\ v_C(4) = 27.97V$$

Example Problem 7

When connected to a 120-Vrms, 60-Hz power line, a load absorbs 4 kW at a lagging power factor of 0.8. Find the value of capacitance necessary to raise the pf to 0.95.



Example Problem 8

A balanced abc -sequence Y-connected source with $V_{an} = 1000 \angle 10^\circ \text{ V}$ is connected to a Δ -connected balanced load $(8 + j4) \Omega$ per phase. Calculate the phase and line currents.

$$V_{an} = 1000 \angle 10^\circ$$

$$V_{ab} = 1730 \angle 40^\circ \text{ V}$$

$$I_{AB} = \frac{V_{ab}}{Z_\Delta} = \frac{1730 \angle 40^\circ}{8 + j4} = 193.4 \angle 13.4^\circ \text{ A}$$

$$I_A = \sqrt{3} I_{AB} \angle -30^\circ$$

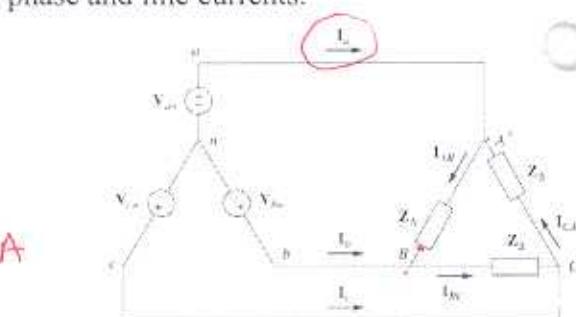
$$= \sqrt{3} (193.4 \angle (13.4 - 30))$$

$$= 335 \angle -16.6^\circ \text{ A}$$

$$I_{AB} = 193.4 \angle 13.4^\circ \text{ A}$$

$$I_{BC} = 193.4 \angle -106.7^\circ \text{ A}$$

$$I_{CA} = 193.4 \angle 133.4^\circ \text{ A}$$



$$I_A = 335 \angle -16.6^\circ \text{ A}$$

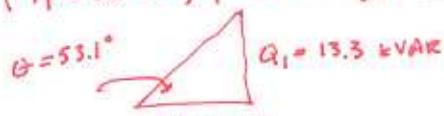
$$I_B = 335 \angle -136.6^\circ \text{ A}$$

$$I_C = 335 \angle 103.4^\circ \text{ A}$$

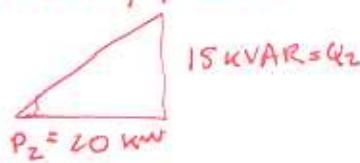
Example Problem 9

Two balance loads are connected to a 240-kV rms, 60-Hz line. Load 1 draws 30 kW (pf=0.6 lagging) while load 2 draws 45 kVAR (pf=0.8 lagging). Assuming the abc sequence determine the (a) the complex, real and reactive powers absorbed by the load, (b) the line currents, and (c) the kVAR rating of the 3 capacitors D-connected in parallel that will raise the pf to 0.9 lagging and the capacitance of each capacitor.

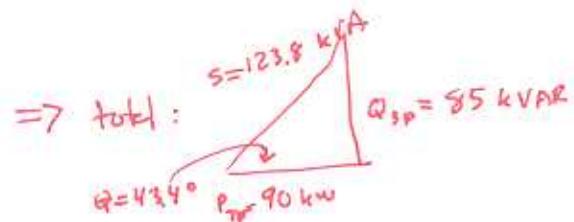
Load 1: per phase ($P_p = 10 \text{ kW}$, $\text{pf} = 0.6 \text{ lag}$)



Load 2: per phase ($\text{Q}_p = 15 \text{ kVAR}$, $\text{pf} = 0.8 \text{ lag}$)



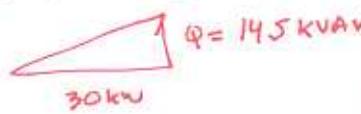
c) combined (per phase) $P_{1p} = 10 + 20 = 30 \text{ kW}$
 $Q_{1p} = 13.3 + 15 = 28.3 \text{ kVAR}$



b) line currents $S = \sqrt{3} V_L I_L$

$$I_L = \frac{123.8 \text{ kVA}}{\sqrt{3} \cdot 240 \text{ kV}} = 0.298 \text{ A}$$

c) to change to $\text{pf} = 0.9 \rightarrow Q$
 $\theta = \cos^{-1}(0.9) = 25.84^\circ$



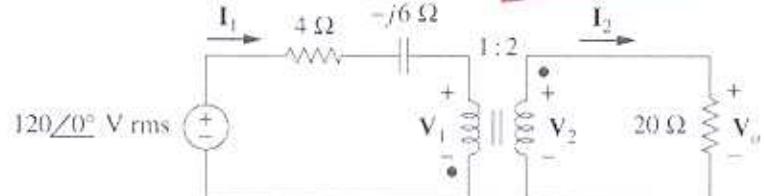
$$\alpha_C = 28.3 - 14.5 = 13.8 \text{ kVAR}$$

$$C = \frac{\alpha_C}{\omega V^2} = \frac{13800}{377(240 \times 10^3)^2} = 636 \text{ pF}$$

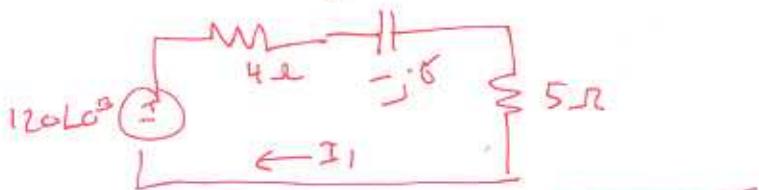
Example Problem 10

For the ideal transformer below find

- the source current I_1
- the output voltage V_o
- the complex power supplied by the source



$$Z_R = \frac{1}{n^2} \cdot Z_L = \frac{1}{2^2} \cdot 20 = 5 \Omega$$



$$I_1 = \frac{120 \angle 0^\circ}{9 - j6} = 11.1 \angle 33.7^\circ \text{ A}$$

$$I_2 = \frac{1}{n} \cdot I_1 = \frac{1}{2} \cdot 11.1 \angle 33.7^\circ$$

$$= 5.55 \angle 146^\circ \text{ A}$$

$$V_o = I_2 \cdot 20 \Omega = 111 \angle -146^\circ \text{ V}$$

$$\vec{S} = \vec{V} \cdot \vec{I}_1$$

$$= (120)(11.1 \angle -33.7^\circ)$$

$$= 1331 \angle -33.7^\circ \text{ VA}$$

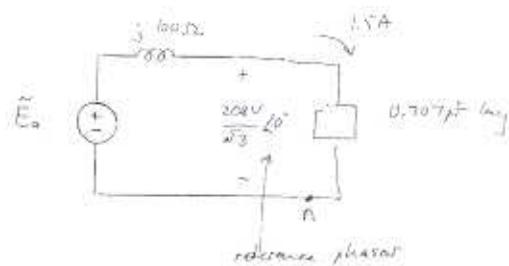
Example Problem 11

A 208-V_{rms} (line), 60 Hz, Y-connected generator has $X_s = 100 \Omega$, $r_s = 0 \Omega$. At rated terminal voltage, the machine delivers 1.5-A_{rms} (line) to a 0.707 pf lagging load.

- Determine the machine current.
- Determine the excitation (or generator) voltage E_a .
- Determine the power (torque) angle δ .
- If the generator has 4 poles, what is the speed of the prime mover?
- Determine the developed torque.
- Suppose the load current increases to 3-A_{rms} at a 0.707 lagging pf. If we have the same terminal voltages, how must the field current change?

a) Load is 0.707 pf lagging $\rightarrow \text{pf} = \cos \theta$
 $\Rightarrow \theta = 45^\circ$

$$I_A = 1.5 \angle -45^\circ \text{ A}$$



b) $\tilde{E}_a = I_A (R_s + jX_s) + \tilde{V}_{AS}$
 $= 1.5 \angle -45^\circ (j100) + 120 \angle 0^\circ$
 $= 249.8 \angle 25.1^\circ \text{ V}$

c) $\boxed{\delta = 25.1^\circ}$

d) $N_m = \frac{120 f_e}{p} = \frac{120(60)}{4} = \boxed{1800 \text{ rpm}}$

e) $T_{dev} = \frac{1}{2} \frac{3V_s E_a}{w_e X_s} \sin \delta = \frac{1}{2} \cdot \frac{3(120)(249.8)}{(377)(100)} \sin(25.1) = \boxed{2.027 \text{ Nm}}$

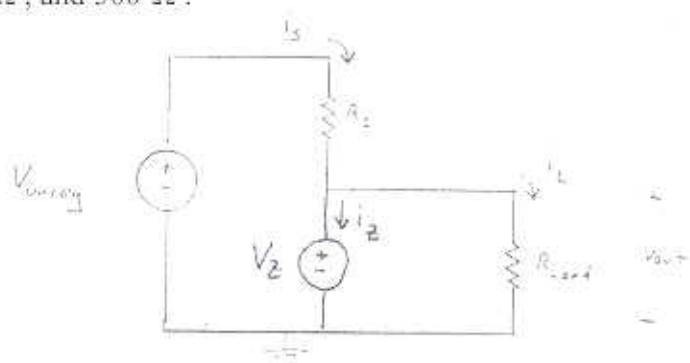
f) See lecture 30 notes ($I_{F2} = I_{F1} \cdot 1.58$)

Example Problem 12

Suppose you choose a 0.5 W, 9 V zener diode for a load application where $300\Omega < R_{load} < \infty$. Determine the range of V_{unreg} for $R_s = 20\Omega$, 100Ω , and 500Ω .

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see next page



Example Problem 12

Suppose you choose a 0.5 W, 9 V zener diode for a load application where $300\Omega < R_{load} < \infty$. Determine the range of V_{unreg} for $R_s = 20\Omega$, 100Ω , and 500Ω .

Step 1: Determine target values for $i_{Z,min}$ & $i_{Z,max}$.

$$i_{Z,max} = 0.8 \frac{P_Z}{V_Z} = 0.8 \frac{0.5W}{9V} = 44.4 \text{ mA}$$

$$i_{Z,min} = \frac{i_{Z,max}}{50} = 0.89 \text{ mA}$$

Step 2: For $R_s = 20\Omega$

$$i_{Z,min} = 0.89 \text{ mA} = \frac{V_{unreg,min} - V_Z}{R_s} = \frac{V_Z}{R_{load,min}} \quad \leftarrow \text{unknown } 300\Omega$$

$$i_{Z,max} = 44.4 \text{ mA} = \frac{V_{unreg,max} - V_Z}{R_s} = \frac{V_Z}{R_{load,max}} \quad \leftarrow \infty$$

$$V_{unreg,min} = 9.62 \text{ V}$$

$$V_{unreg,max} = 9.89 \text{ V}$$

Step 2b: Repeat for $R_s = 100\Omega$ & $R_s = 500\Omega$

$$R_s = 100\Omega : V_{unreg,min} = 12.09 \text{ V}, V_{unreg,max} = 13.44 \text{ V}$$

$$R_s = 500\Omega : V_{unreg,min} = 24.45 \text{ V}, V_{unreg,max} = 31.2 \text{ V}$$

Step 3: Max power dissipated by R_s ?

$$P_{Rs,max} = \left(\frac{V_{unreg,max} - V_Z}{R_s} \right)^2$$

$\underline{20\Omega}$	$\underline{100\Omega}$	$\underline{500\Omega}$
$P_{Rs,max} = 0.04 \text{ W}$	0.197 W	0.985 W

- If we need a smaller ripple for V_{unreg} , need to use larger C .

- Higher ripples causes higher voltage levels and more power dissipation by R_s .

